

EVALUATION OF CONTAINER TERMINAL CONFIGURATIONS BY COMPUTER SIMULATION

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ABSTRACT

With growing ship size and demand for effective handling of container cargoes in recent years, automation has inevitably taken place in almost all aspects of modern terminal operation. So far, automation has been led by the large terminals in Europe and North America and soon it will become a pressure for terminals in developing countries to go for automation. The drawbacks heavily rely on the initial investment cost and a question arises with regard to effectiveness of automation for medium and small size container terminals. A visual environment that simulates container terminal operation is developed to facilitate investigation of advantages and disadvantages of automated container terminal compared to conventional container terminal. A discrete event model for container handling process and agent-based model for path mover flow system is built and validated based on operating terminal in real world and visually simulated to serve the objective. The result of the computer simulation is an evaluation of performance metric for both terminal concepts under similar configurations. In addition, visual simulation was able to notify the area where advantage and disadvantage of both concepts will take place during operation.

Keywords: container terminal, automation, computer simulation, visual simulation environment, performance metric, performance evaluation

INTRODUCTION

The decision to increase ship size by major shipping lines leads to a higher requirement for container terminal. Container terminals have responded to lower growth by investing in handling equipment and IT infrastructure to accommodate larger ships, which pose challenges and require adaptations. Having limited land sources for container stacks and the lack of capability of horizontal transport, maintaining productivity will require dramatic innovation in the handling systems or operational methods and has opened a way for automation to be introduced in recent years (Kim & Lee, 2015). It makes sense for individual players but not for others facing softer annual throughput. Huge investment needs to be made to replace older assets and a lot of complexity has to be taken into consideration to accommodate change or increase terminal capacity.

The main driver for the introduction of automation is to reduce the cost per handled container in the terminal. Other key deciding factors to introduce automation would be reliability, predictability and safety of operations and reduced environmental impact (Cederqvist, 2012). The advent of automation is focused on unmanned container handling equipment process automation in the form of Terminal Operating System (TOS) integration with the information flow from ships, internal and external transportation. While the soft infrastructure of automation can be relatively easier to be

adopted, hard infrastructure of the automated terminal might require a major and significant change to container terminal layout. An automated container terminal mostly use either Automated Guided Vehicle (AGV), Automated Straddle Carrier (A-STRAD) or Shuttle Carrier as their in-yard prime-mover and Automated Stacking Crane (ASC) for yard operation. Conventional yard layout that is parallel to the quay is considered to be outdated and inefficient, and perpendicular to the quay layout has been preferable to minimize the total distance of horizontal transport with heavy burden to the two operating ASCs in each container block.

Most of automated container terminals with perpendicular layout in the world are either located in a strategic hub for an international container trade or a newly built container terminal as an expansion from existing terminal with high annual throughput. On the other hand, layout change is not an easy case for medium and small size container terminals with an annual throughput less than 2 million TEUs. The authors believe that most of container terminal in the world will fall under this category, especially the one with fairly average geostrategic advantage and located in a developing country. This dilemma has been one of the main obstacles to the adoption of automation technology. There are problem of port design and adoption of technology that requires deep understanding on how the current system can work out to cope with challenges and increase its performance with less influence of the physical impact of the automation to terminal layout. An assessment method will be needed to fairly evaluate whether automated container terminal with perpendicular layout is better than conventional terminal with parallel layout.

To address this issue, the paper is constructed in twofold; initiate a benchmarking approach to fairly evaluate performance metrics of layout orientation (parallel or perpendicular to the quayside) using its default configurations and investigate the performance by simulation model based on existing terminal setup. The second section of this paper will briefly explain the layout and configuration of parallel and perpendicular layout as well as introducing performance metrics that needs to be evaluated. The third section deals with conceptual model of the container terminals and simulation setup. The fourth section will discuss the result of the simulation and compare the performance metrics based on the proposed benchmark.

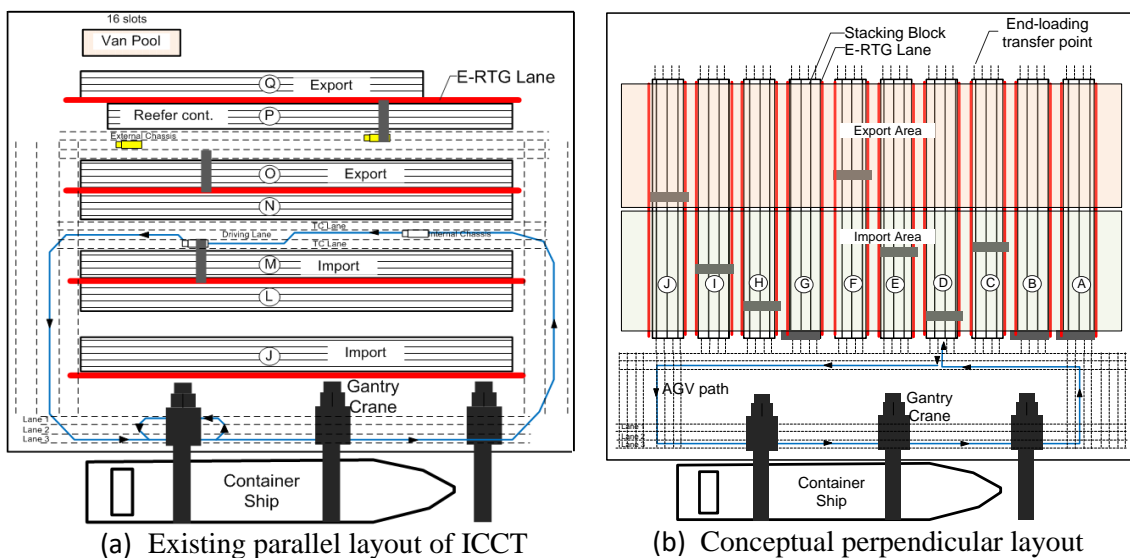


Figure 1. Layout concepts under evaluation

CONTAINER TERMINAL CONFIGURATIONS

Much of the theoretical literature on port planning and performance evaluation are detached from the existing environment with regard to design configurations, handling systems, operating procedures and technology variations (Bichou, 2009). Therefore, this paper will use existing container terminal as the basis of examination to relate theory and port operating practice and show evident regarding to the usability of our approach.

Japan is widely known for automation in its vehicle manufacture industry. However, automation is less utilized for container terminals in Japan. Tobishima Container Terminal in Nagoya City is the only automated container terminal in Japan so far and it still use parallel terminal layout. Perpendicular layout for automated terminal is less preferable mainly because of high initial investment and complex adjustment required for layout modification. Both automated and non-automated terminals utilize similar vertical transport system; Gantry crane for seaside operation and mainly Rubber-Tired Gantry, either diesel powered (RTG), automated (ASC) or Electrified (E-RTG) for container stacking in the yard. For simplification of terms, yard cranes for both systems will be defined as Transfer Crane (TC) in this paper. The major difference of both layouts will be the means of horizontal transport system and layout orientation and transfer points locations of storage yard as shown in Figure 1.

Parallel Layout

The terminal configurations explained in this section use the terminal layout and cargo handling equipment configuration of Island City Container Terminal (ICCT) in Fukuoka City – Japan. The yard configurations in ICCT consist of truck-chassis wheeled system as prime-mover for horizontal transport within the terminal. The storage yard operation is based on sharing policy of RTG which allows RTG to move around different yard blocks without restriction. Since ICCT utilize E-RTG type of TC for yard operation, there is electric tray with steel structure system bolted on top of a concrete base at one side of each container block. Electrical energy is picked up from the conductor rails using a collector trolley connected to the TC. Therefore, only one TC is usually placed in one container block at a time due to restriction of electric consumption of the terminal. The container stacking sequences in the yard is usually pre-determined by scheduler in a way that TC movement along the block is minimized.

Vertical Layout

The concept of automated container terminal investigated in this paper is based on EUROMAX container terminal layout where orientations of stacks are arranged perpendicular to the quay. We brought the layout concept and stack orientation and implement it in accordance to the basic terminal dimension of ICCT. The horizontal transport of containers between the quay and the storage yard is carried out by Automated Guided Vehicle (AGV). AGV are similar to conventional trucks-chassis system but operate on a pre-defined guide path without drivers. Each block in the container storage yard is occupied with at least two ASC type of TC serving at both end of the block for import-export containers (seaside operation) and receipt-delivery containers (gate operation). As opposed to the parallel layout, the number and location of yard transfer points (TP) is significantly different. There are 4 TP placed at every end of each blocks. Due to the smaller of TP attached to a block and the orientation of the block significant increase of total covered distance of TCs is expected to happen.

Table 1. Performance metrics to evaluate parallel and perpendicular terminal layout

No	Performance metrics	Definition of metrics	Measured dimensions
1 Gantry crane (GC) metrics			
a.	Productivity	Number of handled container by GC.	Unit (Box/hour/GC)
b.	Waiting time	Time spent by GC to wait for prime mover arrival.	Unit (sec/box)
2 Prime mover (PM) metrics			
a.	Working time	Time required for prime mover from picking up container from GC and travel until reach yard transfer point (TP). This measurement is not including the time prime mover spent when travels in empty condition.	Total (sec) Average (sec/pm), Unit (sec/box)
b.	Moving time	Time where the prime mover are moving during simulation. Measured in total (hour) and average (hour/prime mover)	Total (hour) Average (hr/pm)
c.	Covered distance	Distance covered by prime mover during simulation.	Total (km) Average (km/pm)
d.	Idle time	Idle time of prime mover is parked and waiting for a task to be conducted.	Total (sec) Average (sec/pm)
e.	Wait time to transfer	Time spent by prime mover waiting to transfer container to TC. Measured in Total (sec), average (sec/prime mover) and unit (sec/prime mover/box)	Total (sec) Average (sec/pm), Unit (sec/pm/box)
e.	Time in motion	Total percentage of situation where TC is in a motion during the simulation run.	%
3 Transfer crane (TC) metrics			
a.	Working time	Time required for TC from picking up container from prime mover and stack container to designated location. This measurement not including TC retrieval time on empty condition.	Total (sec) Average (sec/TC), Unit (sec/box)
b.	Covered distance	Total horizontal distance covered by TC during simulation	Total (sec) Average (sec/TC), Unit (sec/TC)
c.	Time in motion	Total percentage of situation where TC is in a motion during the simulation run.	%
4 Overall handling metrics			
a.	Service time	Handling time of container from ship to stacking location for import operation during the simulation run.	Total (sec) Unit (sec/box)

Benchmarking Operational Performance

The goal of every container terminal is to perform efficiently and maintain competitiveness by providing low cost and high quality services to customers. In import container operation case, the container ship's berthing time has to be minimized. In other word, designated GCs have to operate at the maximum productivity during the work shift. Performance metric of container terminal is a numbers game with all important throughput figures often featuring as benchmarks. There is not a single holistic benchmark that can be applied asses a container terminal performance. Therefore, carefully identifying characteristics of the handling activity should lead to more accurate indicators and targets. This paper focuses on terminal productivity issue that covers all issues driven by the detail performance of container handling equipment used in both parallel and perpendicular layout. We present the performance criteria that are used to evaluate advantage and disadvantage between those two layouts in Table 1. Aside from commonly used metrics, we add new metrics that will show the difference of both layouts in terms of equipment utilization that will closely relate to the performance of local system in respect to global productivity of container terminal.

SIMULATION SET UP

Simulation models have been used intensively to understand the behavior and test different strategies in the container terminal systems, e.g. see (Hayuth et al., 1994; Yun and Choi, 1999). These simulators differ widely in objectives, complexity, and details. Liu et.al. (2004) developed a simulation model used to demonstrate the impact of AGV deployment for parallel and perpendicular terminal layout and used multi attribute decision making to assess the performance. The result showed that the use of AGV brings substantial performance effect to container terminal and has different effect considering different terminal layout. Taner et.al. (2014) obtained similar result from by examining the effect of dispatching rules and resource allocation strategies specifically for perpendicular layout of automated terminal. Both papers showed that each layout format requires a unique combination of cargo handling machineries. However, detail performance benchmarks for both layouts were not presented.

In this paper, we will evaluate only the import operation (incoming containers from ship) and see how various configurations work to get every performance metrics that we desired. The main performance metric that should be achieved is to reach optimum gantry crane productivity under a ship working shift where other metrics will be shown as the byproduct of that effort. Duration of simulation is fixed to 8 hours (terminating system) according to actual work shift of equipment in the container terminal. The input data of the import containers is generated in advance based on actual unloading sequences. Pseudo-random numbers are used to generate loading sequence so that the results for a given scenario can be reproduced. A unique container number, unloading sequence and stacking position are generated using Mersenne Twister algorithm introduced by Matsumoto & Nishimura (1998) which completely independent of one another.

By iteratively checking flow of input and quality of output data as well as using simulation animation, we were able to detect actions that are illogical to ensure that the simulation model accurately reflects the conceptual model and then fix the computer model. We simulate 5 numbers of replications for each simulation setup, compute the sample variance of the selected estimate, and have determined that the width of the resulting confidence interval is within acceptable limits.

Modeling Terminal Layout and Configuration

In port operations and management, modelling has proven to be a powerful tool to design and analyze real world complex situations. Our approach use 3D model in constructing container terminal model made us able to make a detail model of every system in the terminal e.g.; gantry crane system, prime-mover system, transfer crane system and the connection between those systems. We use AutoMod, a general simulation software with 3D model construction and visualization capability for discrete event simulation. There are four layout and configuration models that has been built and simulated as shown by Figure 2. Two models for parallel layout: Parallel_6TC_6Lane (Model A) and Parallel_6TC_3Lane_Landside (Model B) and two models for perpendicular layout: Perpendicular_6TC_6Lane (Model C) and Perpendicular_6TC_3Lane (Model D). The equipment configurations for both layouts are as follows.

Parallel layout model configuration

For parallel layout, we assume that two gantry cranes (GC) are serving a container ship at the berth. Model A serves as the basic model to be evaluated against anoter models. For the experimentation purpose, only one ship berth and six container

blocks/lanes (24 bays x 6 rows x 4 tier for each) in the coverage area of the berth will be examined and considered as the basic terminal dimension to be compared with perpendicular layout. In addition, 24 container transfer points (TP) are set on the side of each block. Normally, the export containers are placed closer to the berths and import containers are placed closer to the land side. This setup makes truck-chassis transporting import containers travels a longer distance than it should be. For evaluation purpose, two stack location models were built; Model A utilize a default 6 storage block with one operating TC on each block currently used by ICCT. We investigate the possibilities of increasing terminal performance by increasing the number of TC working in a storage block at the same time. Therefore, Model B configured to use only 3 blocks on the land side of the terminal (Figure 2b), as a measure to increase TC productivity.

The number of truck-chassis deployed in the system move in a counter-clockwise loop between the quay and the stack and the amount were varied from 2 to 12 units for every simulation. The truck-chassis served by the GC and TC based on the first-come-first-served (FCFS) rule. It is also assumed that at most six truck-chassis are allowed to wait in any GC queue at each instant of time. In actual operation, truck-chassis may be allowed to travel up to 30 km/h. In this paper however, it has a forward speed limitation of 22 km/h to be same with AGV maximum speed.

Perpendicular layout model configuration

GC configuration for perpendicular layout is exactly the same with the one used for parallel layout. The storage area configuration is configured as follows. Ideally, one storage block will have 4 transfer points (TP) to synchronize container transport from AGV to TC. Considering the layout configuration of parallel layout, modifications were made to fairly compare both layouts. The first model utilizes 6 storage blocks that use one TC and have only one TP on each (Figure 2c). The second model utilizes 3 storage blocks that use one TC and have two TP on each (Figure 2d). For both model, only 12 bay lengths on each block are active for import container stack out of 24 bays. We also tried to add an innovated concept of yard container transfer that has been introduced in several automated container terminals, e.g. docking station as illustrated by Figure 3. The key of this concept is to provide buffer area where AGVs can unload a container without having to rely and wait on TCs so it can perform the next task without delay.

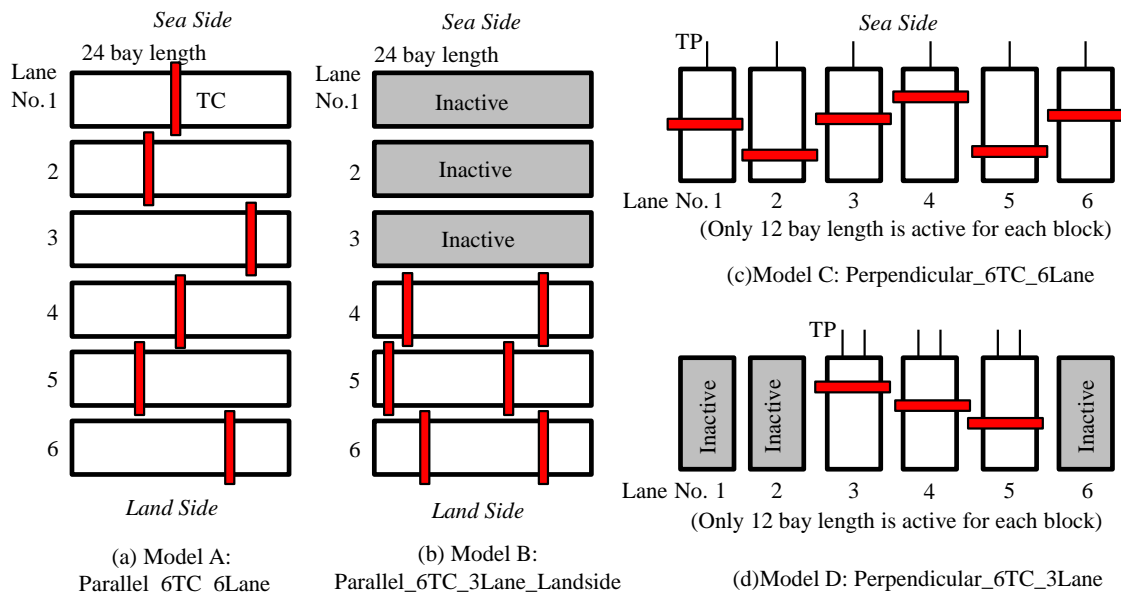


Figure 2. Terminal layout and configurations tested with simulation

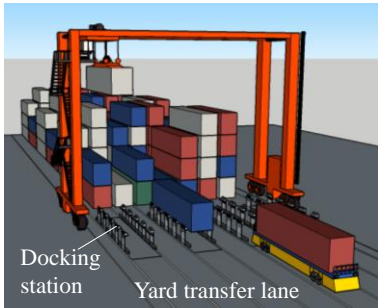


Figure 3. Docking station at yard transfer point

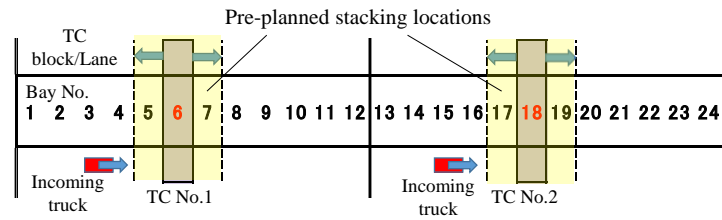


Figure 4. Stacking strategy for parallel layout to minimize TC movement

The AGV configuration is also mostly similar to truck-chassis configuration for parallel layout. The different is that the AGV is moving freely in the seaside area after catching container from GC and find the closest path to the transfer point destination attached to a designated block. AGVs do not have to follow specific loop in order to transport import containers. Furthermore, AGVs can travel forwards, in reverse and can overtake each other. The technical parameters and dimension of the working AGV in this paper follows the parameters used in Široký (2011). It is 14.8 m in length and 3 m in width, making it able to transport containers of different length up to 40'. The maximum forward/reverse speed is 22 km/h with stopping distance of 5 m when facing other AGV passing by, while curve speed is set to be 11 km/h at the maximum. AGV is also served by the GC and TC based on the first-come-first-served (FCFS) rule.

Simulation Logic

The developed AutoMod models contain several local systems and collections of entities. The process system defines the model logic that controls how loads are processed in a model. The simulation logics for every local system (GC, Prime-mover, TC) and synchronization rules between moving entities controls how containers are processed in a model. In this section, we briefly explain the logic used to do make stacking strategies for both layout and logic to conduct traffic management for AGV in perpendicular layout since those requires special attention.

Stacking strategy in storage yard for parallel and perpendicular layout is different, showing how layout orientations have an impact to stacking strategies to maintain stack efficiency and minimize future re-handling. We mimic the parallel layout stacking strategies performed by stack planner in ICCT where a given area in a block are prepared in advance to store import containers to minimize TC's horizontal motions as shown by Figure 4. On the other hand, stacking location for import containers in perpendicular layout can be any given stack positions within the center any container block length to the end of that block on the quay side.

AGV flow in perpendicular layout is somewhat complicated unlike truck-chassis loop flow in parallel layout. Due to the nature of the layout, AGV traffic is inevitable. AGVs may cross-passing each other and deadlock condition might happen. To alleviate this, three traffic management solutions are being implemented e.g.; collision avoidance, dispatching rules and routing. A specific collision avoidance rule based on hierarchical system called semaphores introduced by Evers and Koppers (1996) is implemented to the simulation logic to control the moving traffic. Furthermore, dispatching rules of AGV is set based on the availability of AGV and the readiness of container to be transported from the GC. An empty AGV will change status from "work" to "idle" and travel to buffer area in between the quay and stacking yard. This

buffer area has several slots and only one empty AGV can claim the slot at an instant time. Then the AGV that has arrived at the buffer area will be placed at the end of vehicle waiting list to be notified when any container is ready to be picked up.

Finally, routing of AGV is done by placing traffic control points in the prime-mover sub system. AGV Paths are drawn using different primitives (straight sections, curves etc.) and control points for interaction are snapped on them. Each control point can only be assigned to one path (Gutenschwager et.al., 2012). After confirming a shortest route to destination using Dijkstra's algorithm, any moving AGV have to claim a control point on every path along the route and release it after passing the path. Every control point has claiming capacity of 1, means that once it has been claimed by an AGV, the second AGV tries to claim the same control point has to wait on its current position until the control point has been released by the first AGV, or find another control point to be claimed and re-routes from its original route. These procedures evolve over time as the simulation runs to alleviate deadlock condition.

RESULTS AND DISCUSSION

Comparing Handling Equipment's Productivity

The analysis of simulation output begins with the selection of performance measures. There are six selected performance metric used to benchmark existing non-automated terminal configuration (Model A) with three proposed conceptual layout orientation and configuration of automated container terminals.

GC productivity for all evaluated models is shown in Figure 5. This is main performance metric showing the amount of container handled by one GC per one hour. Reaching maximum GC productivity at 40 box/hr is important since it will directly correlate to ship's berthing time. Obtaining GC maximum productivity will also means that GC doesn't have to wait for prime-mover arrival, and there is no waiting time of GC. Therefore it is safe to assume that GC waiting time as shown in Figure 6 is directly related to the GC productivity. Refer to Figure 5, Model A and B reach maximum productivity utilizing 6 truck-chassis, while Model C case needs 8 AGVs, and Model D case needs more than 12 AGVs. This result inferred that Parallel layout is more efficient than Perpendicular layout from prime-mover installation cost perspective. Furthermore, Model D case doesn't reach GC maximum productivity of GC even after utilizing 12 AGVs, due to lack amount of TC being utilized. Even in case of using docking station, the stations have a limited capacity. Having to wait for TC to pick up container docked at any station, incoming AGV with container on it will have to wait until docking stations are available. However, due to less amount of TC is required for Model D compare to the other model, cost advantage from lower number of TC exceeds disadvantage of GC productivity, then Model D case might become adequate choice when GC maximum productivity is not become the main target of operation.

Unit service time is shown by Figure 7. Unit service time is total duration that is needed to handle one container from ship stowage to designated stacking location in the storage yard. So, unit service time shows the whole utilization of cargo handling equipment required to transport a single container. It also shows efficiency of each handling case. For instance, unit service time of Model B is higher than model A in any number of truck-chassis configuration. This is because stacking lane is unevenly distributed to the land side in Model B and truck-chassis need to run long distance on average compare to Model A. Consequently, unit service time of parallel layout models (Model A and B) is generally lower than that of perpendicular models (Model C and D).

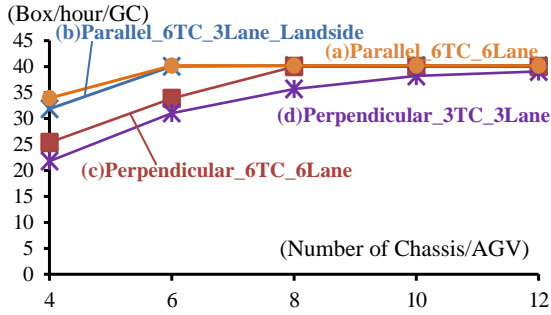


Figure 5. GC Productivity

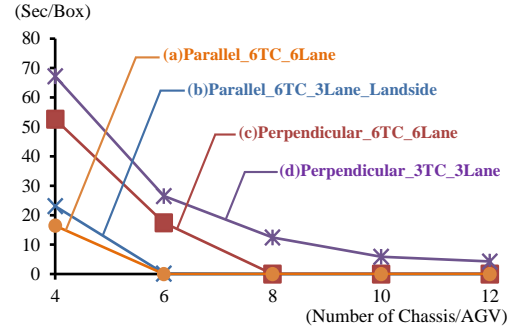


Figure 6. Unit GC waiting time

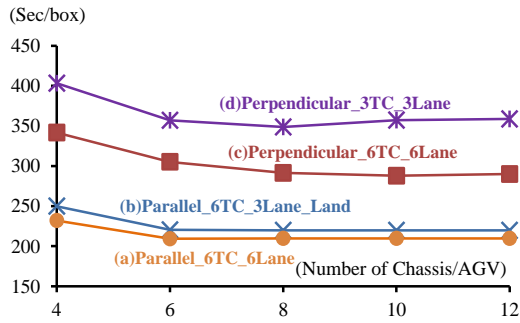


Figure 7. Unit service time

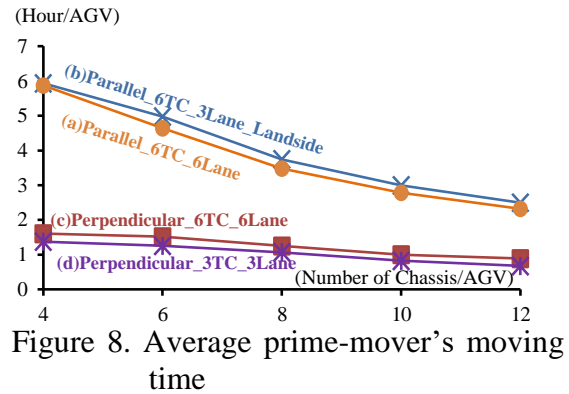


Figure 8. Average prime-mover's moving time

This result shows that parallel layout is more effective than perpendicular case from the speed of container handling perspective. However, this parallel model's unit service time is shorter than required to maximize GC handling productivity. A fair analysis can be drawn by examining the simulation animation. When the deployed number of prime-mover is 8, GC handling productivity for Model A, B and C is 40box/hour/GC and there is no GC waiting time, but, unit service time of Model C is about 300 second. On the other hand, unit service time of Model A and B is about 220 second. This means that the unit service time for perpendicular layout using Model A is enough to maximize GC handling while unit service time for parallel layout is too shorter than that is needed.

Average prime-mover's moving time is shown by Figure 8. Using this metric, prime-mover expected energy consumption can be evaluated. Furthermore, Chassis and AGV utilization rate can be confirmed. If this moving duration is low, then that means that prime-mover is idling or stop for long duration. From Figure 8, it can be concluded that truck-chassis moving duration of each parallel layout models is longer than AGV moving duration of perpendicular layout models. This is mainly due to the difference in prime-mover moving path that comes as the consequences of layout orientation and yard transfer point locations. Shorter path of AGV is one of advantage of perpendicular layout. However, low moving time is also means that AGV stop and wait for long time and AGV usage rate in perpendicular case is lower than truck-chassis usage rate in parallel case. Incidentally, Chassis energy consumption rate and AGV energy consumption rate that based on moving duration is different. Therefore, it is impossible comparing truck-chassis and AGV energy consumption only from Figure 8.

In addition, truck-chassis moving duration in parallel layout models is decrease with the increase number of truck-chassis being deployed. This is not the case for perpendicular layout models. AGV moving duration does not decrease with the increase number of AGVs as much as parallel case. Prime-mover total distance for all models is shown by Figure 9. It shows the merit of perpendicular layout in terms of reducing

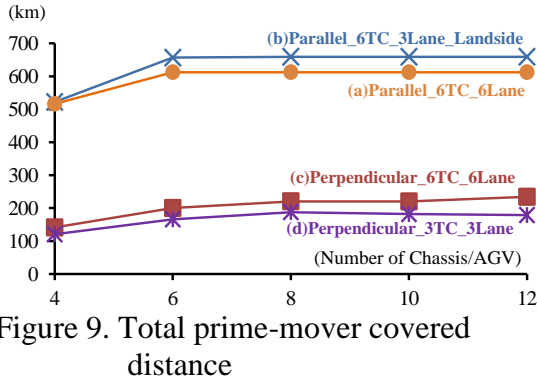


Figure 9. Total prime-mover covered distance

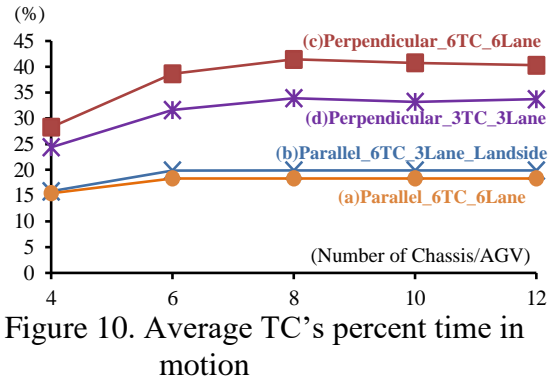


Figure 10. Average TC's percent time in motion

horizontal distances that have to be covered by prime-mover for various setups. The total covered distances are saturated after utilizing some number of prime-movers in the system. Correlating this finding to Figure 5, it is safe to conclude that prime-mover's deployment above a certain level would not be necessary since GC productivity would not be increase further. In addition, this metric can be used to calculate prime-mover energy consumption in pair with Figure 8.

Last metric explained in this paper is the average TC's percent time in motion shown by Figure 10. This metric is unique because it covers the duration percentage of each TC move in any mode of TC work in its moving sequence e.g. horizontal movement to retrieve, picking-up container from AGV by trolley, horizontal movement to delivery and container set-down by trolley at designated stack location. In other word, this metric shows how TC is affected by layout orientation and equipment configuration. Therefore, utilization rate of TC is able to evaluated by refer to this metric. From Figure 10, TC percent time in motion for Model B is slightly higher than that of Model A. This implies that the TC utilization rate for parallel layout can be increased by using two TC operates at the same container block/lane. This finding is important to be disclosed to terminal operator searching a measure to increase their productivity by TC dispatching strategy. On the other hand, TC percent time in motion for Model C is higher than that of Model D. This finding shows that the efficiency of perpendicular layout utilizing smaller amount of container block/lane will be lower, even when the number of active transfer points and docking stations is increased.

By pairing Figure 5 and Figure 10 we can draw a general conclusion regarding TC utilization rate. Note that maximum GC productivity can be reached by deploying 8 prime-movers for Model A, B (parallel layout) and C (perpendicular layout). In this case, TC motions can be inferred as the amount of energy consumed by TC. To reach the same amount of productivity, note that the single TC in perpendicular layout is expected to consume more energy due to its higher percentage in motion compare to a single TC in parallel layout. Again, due to the nature of the layout shown by Figure 1b and Figure 2c, a TC in perpendicular layout has to go back to the end side of a container block/lane to retrieve container from the docking station. This retrieval operation that consumes energy is alleviated in case of parallel layout because a stack area that closes to one another can be prepared in advance to minimize TC horizontal movement as shown by Figure 4. On different point of view, TC percent time in motion can also be cross-interpreted as TC utilization rate. In this sense, one can point out that TC usage rate for parallel models may be lesser than that of perpendicular models. Amount of TC and performance is a trade-off in operation and we might be able to decrease the number of TC being utilizes with an awareness to keep GC under its maximum productivity.

CONCLUSION

Adoption of dramatic innovation in the handling systems such as automation technology in container terminal is a difficult task for terminal having softer annual throughput compared to major terminal players. Hard infrastructure of the automated terminal might requires a major and significant change to container terminal layout. In this paper, we investigated, through developing benchmark for measuring performance metrics as well as simulation models, the impact of layout orientations and terminal configurations on overall performance of container terminal systems.

An existing layout and configuration is compared with three conceptual models incorporating stacking allocation strategy, vehicle dispatching strategy and the use of different non-automated and automated cargo handling equipment. We showed the merit of perpendicular layout in automated terminal in comparison to parallel layout in non-automated terminal in terms of minimizing horizontal transport as well as its disadvantage in terms of heavy burden given to yard transfer crane. Based on the findings, a research agenda can be made in order to examine a way to reduce the burden of yard transfer crane in automated container terminal utilizing perpendicular layout.

Apart from the automation technology, yard layout has inevitable effects to the terminal performance due to effort that has to be made by handling equipment to reach optimum productivity. Our result also shows that configuration of two transfer crane serving at the same parallel storage block show a great promise in increasing existing container terminal productivity.

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